

REKABENTUK SISTEM KERANGKA KONKRIT PRATUANG.

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CKAS JKR

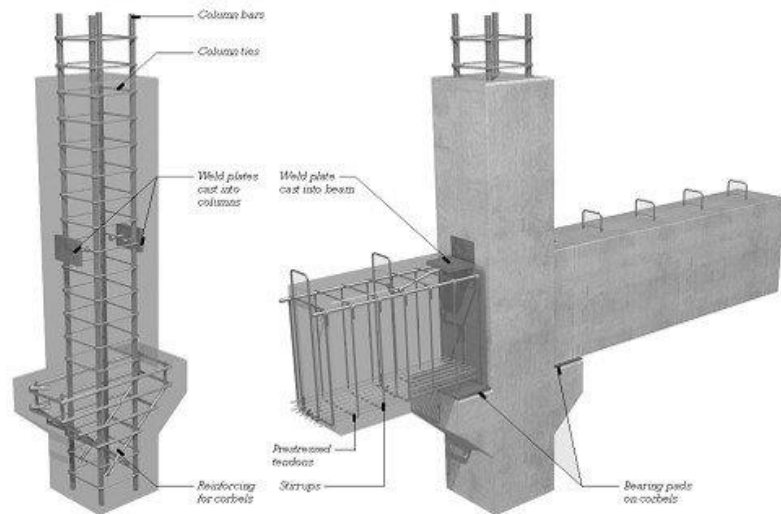
REKABENTUK SISTEM KERANGKA KONKRIT PRATUANG.

1. Prinsip rekabentuk bangunan konkrit pratuang.
2. Kod amalan rekabentuk.
3. Stability kerangka (*Frame Stability*)
4. Sistem kerangka konkrit pratuang
5. Rekabentuk braced component (*Shear wall*).
6. Ties and Connections to braced structure.

Prinsip rekabentuk bangunan konkrit pratuang

- Perbezaan bangunan konkrit insitu dan pratuang adalah pada sambungan (connectivity)
- Sambungan bangunan konkrit insitu berlaku semasa semasa kerja konkrit berjalan.
- Untuk struktur pratuang, sambungan berlaku apabila komponen struktur seperti tiang/rasuk, papak/rasuk disambungkan.
- Kelakuan struktur sepertimana direkabentuk.

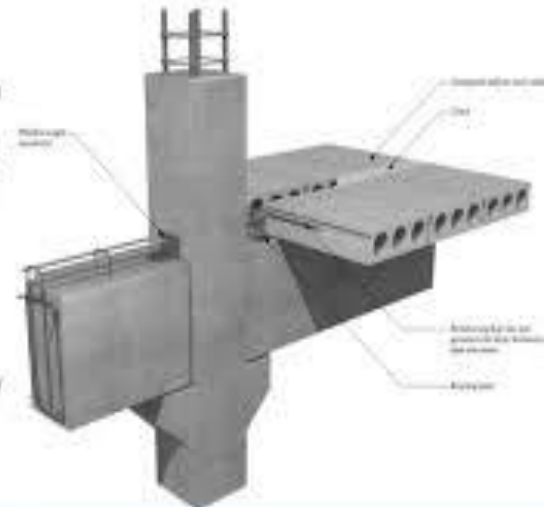
BEAM TO COLUMN CONNECTION



JOINING PRECAST CONCRETE ELEMENTS

Example Slab-to-Beam Connection

- Hollow core slabs are set on bearing pads on precast beams.
- Steel reinforcing bars are inserted into the slab keyways to span the joint.
- The joint is grouted solid.
- The slab may remain overlapped as shown, or topped with several inches of cast in place concrete.



- The behaviour of the precast structure is dependent on the behaviour of the connections.
- It respond to
 - Resistance to all design forces
 - Ductility to deformations
 - Durability
 - Fire resistance
 - Production and construction consideration

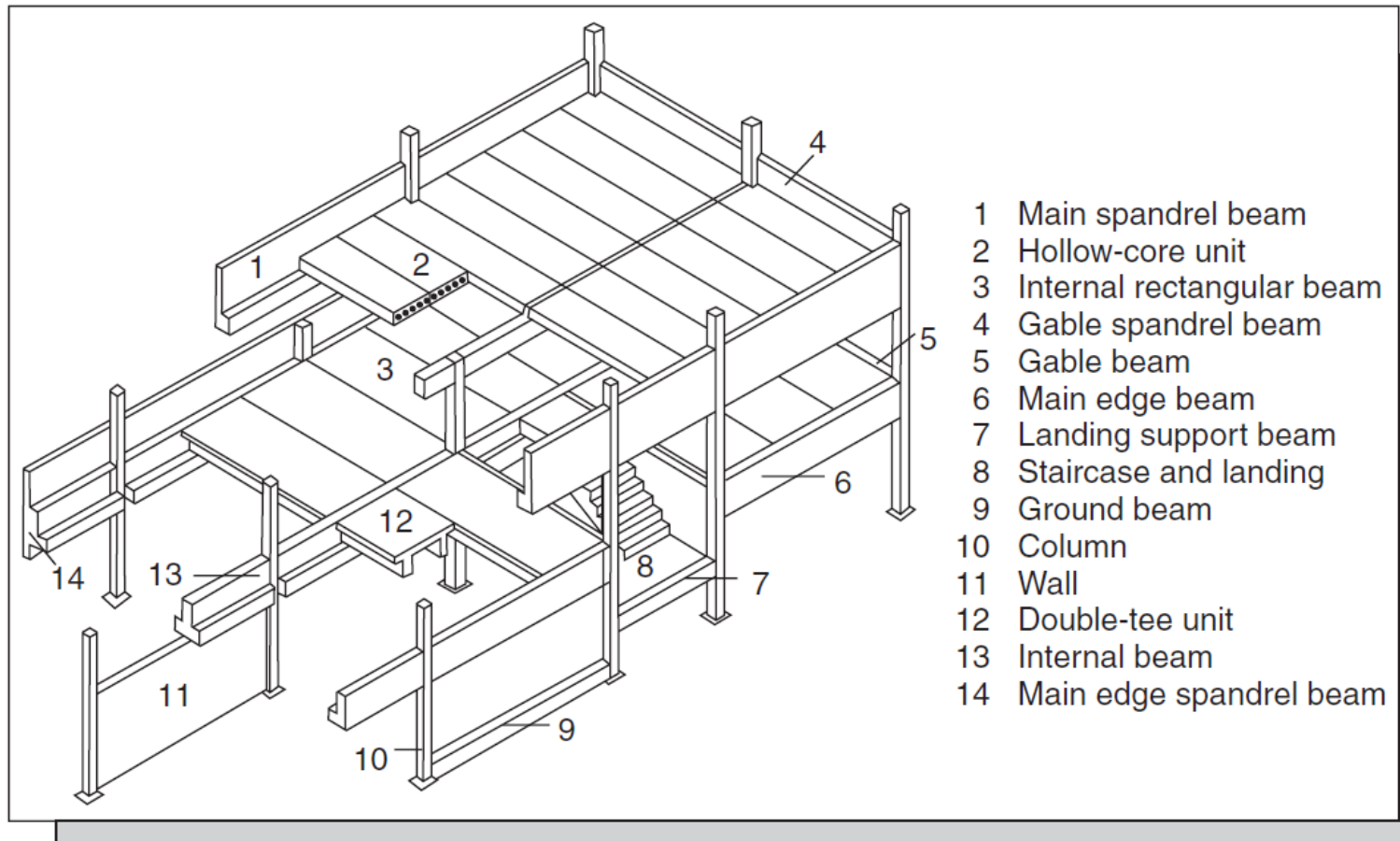


Figure 3.2: Definitions in a precast skeletal structure.

Types of Structural Systems in Precast Concrete Structures

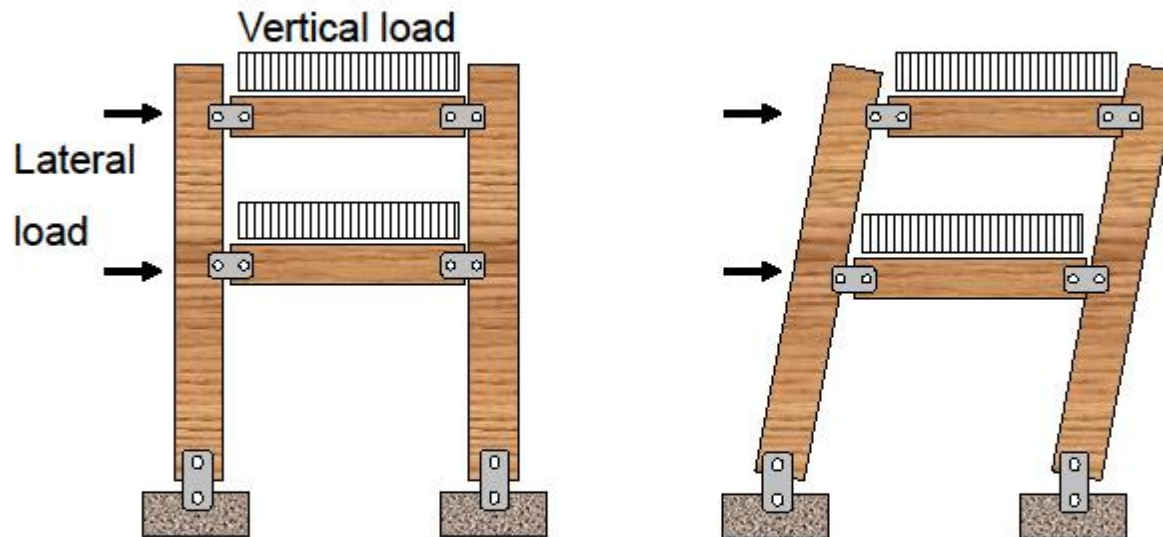
Wall System (Load bearing system)



Skeletal frame system

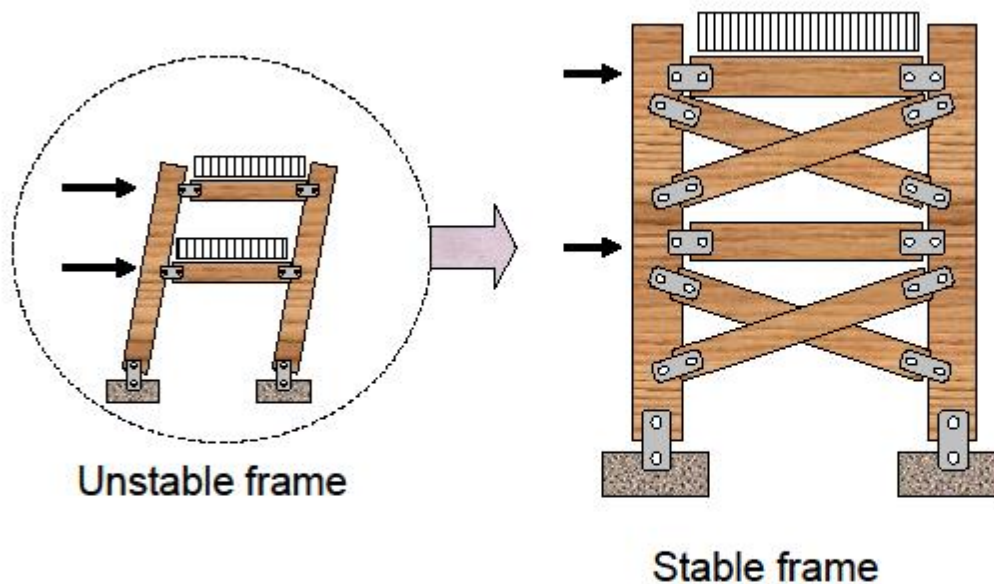


Frame Stability



- Pinned beam-to-column connections
- Frame is not stable when subjected to lateral forces.

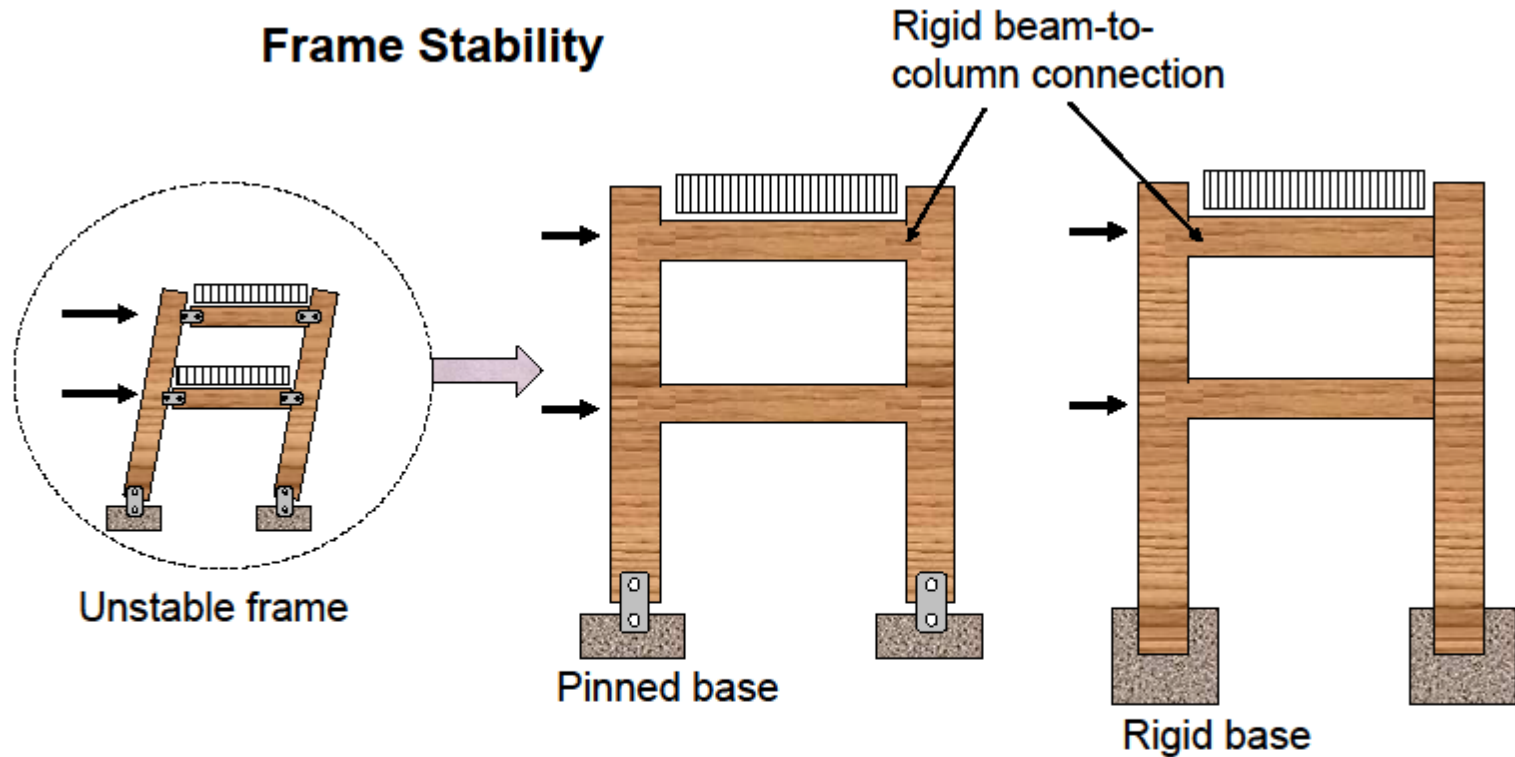
Frame Stability



Methods to stabilize the structure:

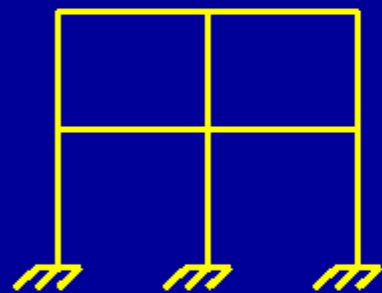
- Introduce bracing system
- The system is known as Simple Construction System

Frame Stability

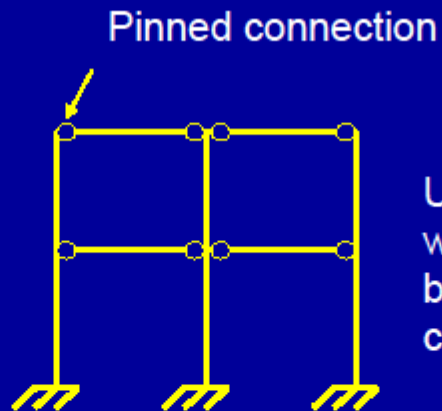


Methods to stabilize the structure:

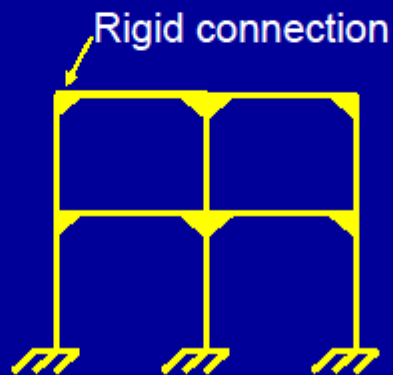
- Introduce rigid beam-to-column connections
- Column-to-base connection can be pinned or rigid



**Unbraced
frame**



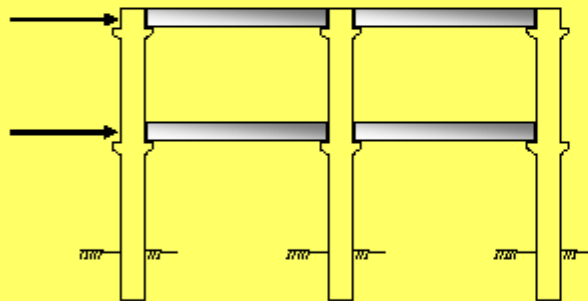
Unbraced frame
with pinned
beam-to-column
connections



Unbraced frame
with rigid beam-
to-column
connections

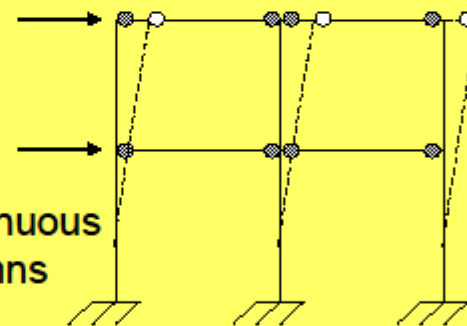
Frame Action - Cantilever column

Typical frame model
for analysis



Pinned beam-to-column
connections

Continuous
columns



Fixed bases

Frame Action - Cantilever column

Cantilever column:

- **Low-rise skeleton structures are normally stabilized through the cantilever action of the columns.**

Frame Action - Cantilever column

Criteria for unbraced frames with cantilevered columns

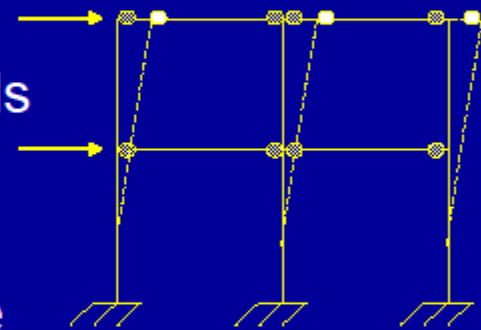
- ***Beam-to-column connections are assumed as pinned.***

Any partial restraints provided by the beam-to-column connections, walls or spandrel panels are ignored.

- ***Column-to-base connections are fixed.***

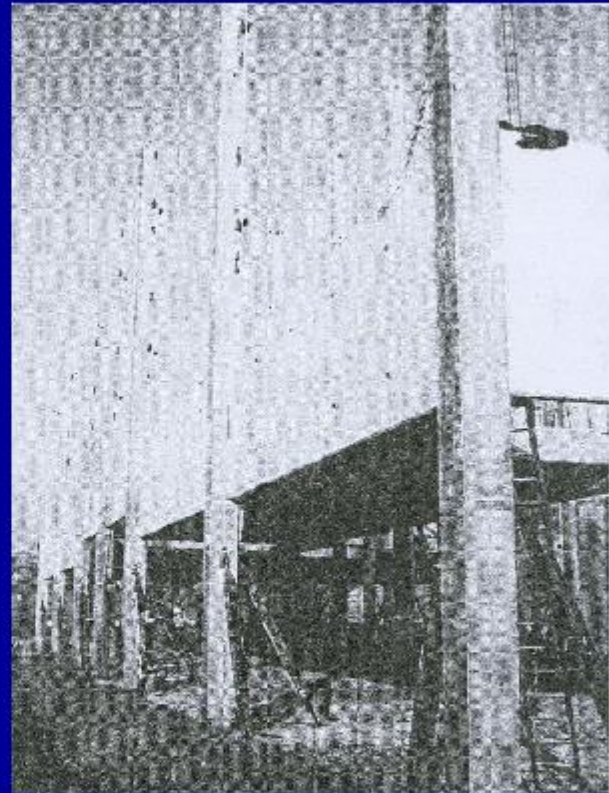
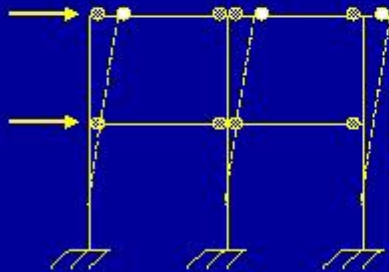
The precast columns are fixed into the foundations with moment-resisting connections. As a result, columns can be analyzed and designed as cantilevers

- ***No other independent lateral resisting systems such as shear walls or cores.***



Frame Action - Cantilever column

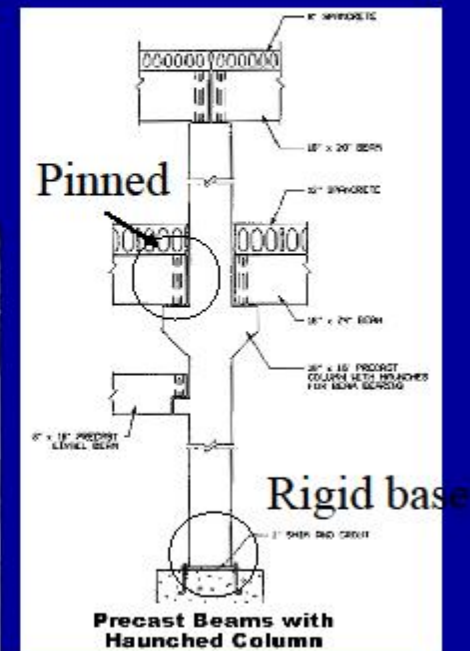
- The stability of unbraced pin jointed frames is provided entirely by columns designed as cantilevers for the full height of the structures.



Typical example of unbraced frame with cantilever columns

Frame Action - Cantilever column

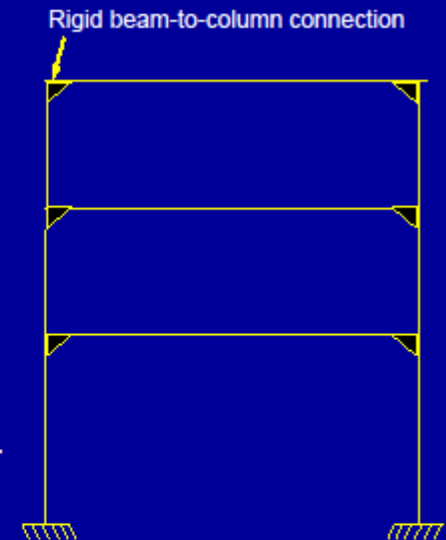
- Other examples where the stability of unbraced frames against lateral forces can be achieved by the designing the columns as cantilevered.



Frame Action – Moment Resistance Frame

Criteria for unbraced frames with frame resistance action

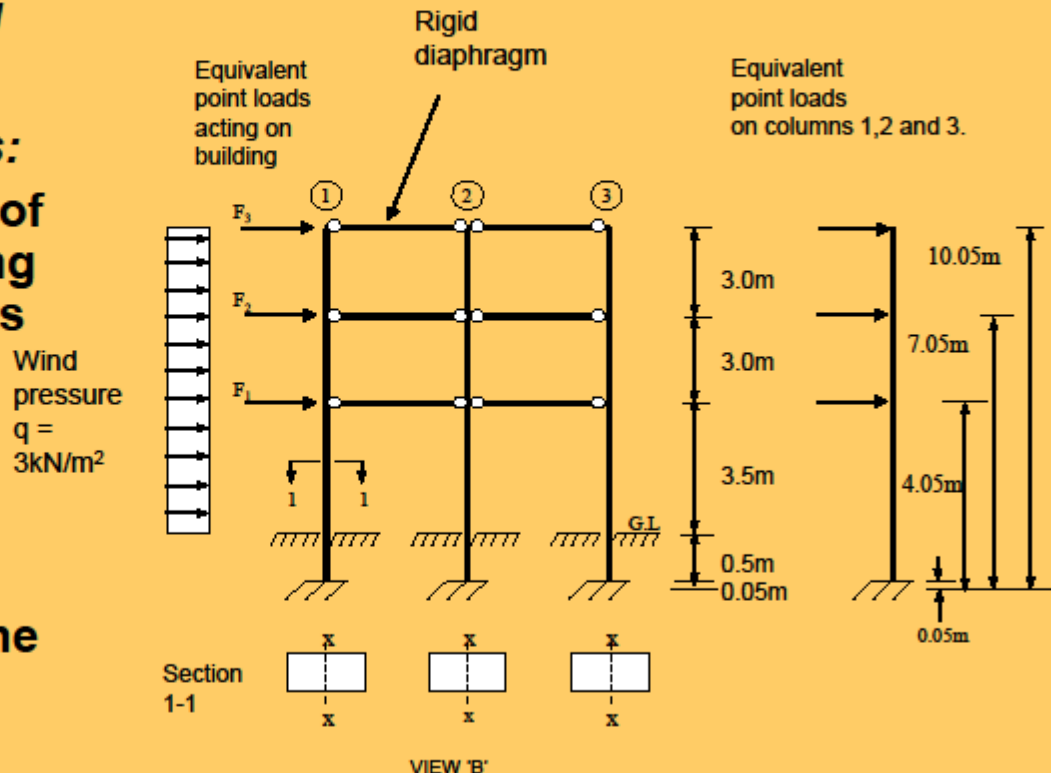
- ***Beam-to-column connections are assumed as rigid.***
Restraints provided by the beam-to-column connections are considered in the analysis and design.
- ***Column-to-base connections are fixed.***
- ***No other independent lateral resisting systems such as shear walls or cores when lateral deflections are not excessive (i.e. in the case of low storey frames).***



Frame Action - Cantilever column

Analysis of lateral loads for unbraced frames with cantilever columns:

- The distribution of horizontal loading between columns is directly proportional to the second moment area of the columns, I .
- In most cases, the columns will be equally loaded horizontally.



Frame Action - Cantilever column

Limitation:

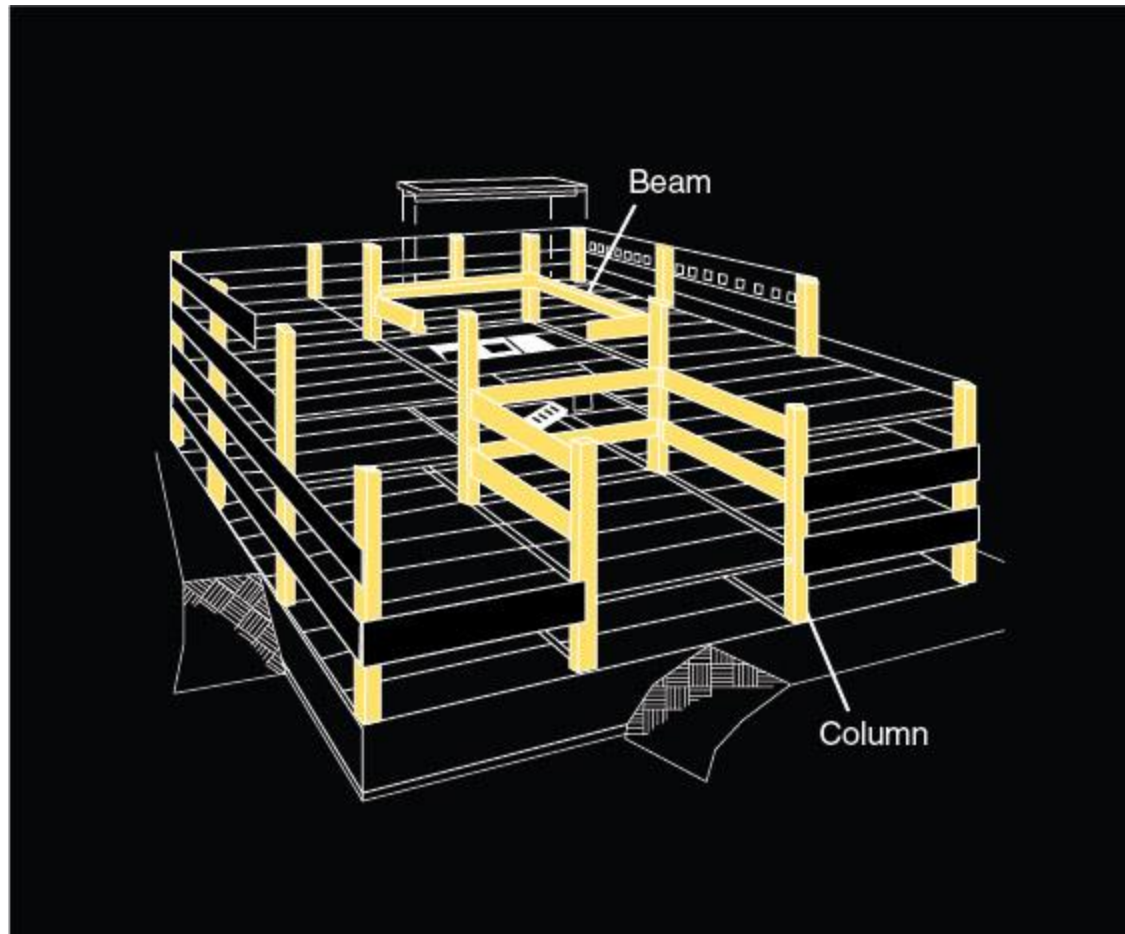
- **The maximum height of an unbraced frame with cantilever action is 10m (i.e. up to about 3 storeys).**
- **Cantilever columns are designed using effective length factor of 2.3, hence larger columns.**

Advantages:

- **No bracing**
- **Pinned beam-to-column connections – simple to construct.**
- **Columns are manufactured in a single length, column splices are not required.**

Unbraced Frame





Moment-Resisting Frames

Moment-resisting frames are those in which a degree of rotational restraint is provided between vertical components (usually columns) and horizontal components (usually beams and/or spandrels). This system then resists lateral loads imposed on the structure.

Frame Action – **Moment Resistance Frame**

- The stability of unbraced rigid frames is provided by the bending resistance and the rigid connections.

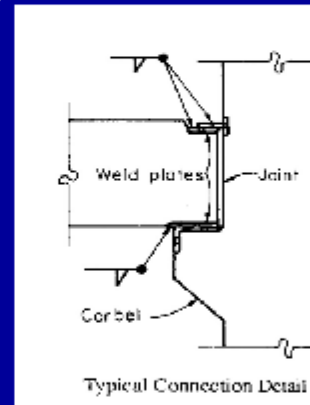
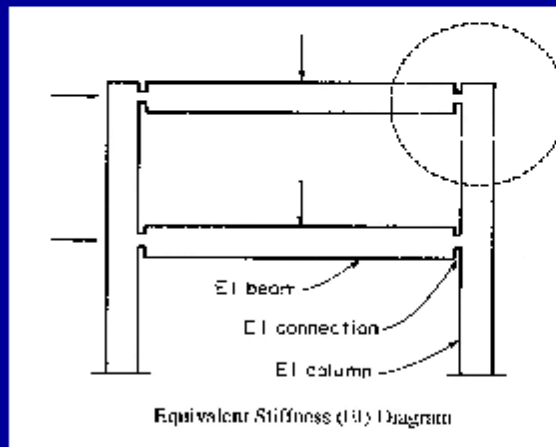


Rigid beam-to-column connections

Typical example of unbraced precast frame with rigid beam-to-column connections

Frame Action - Moment Resistance Frame

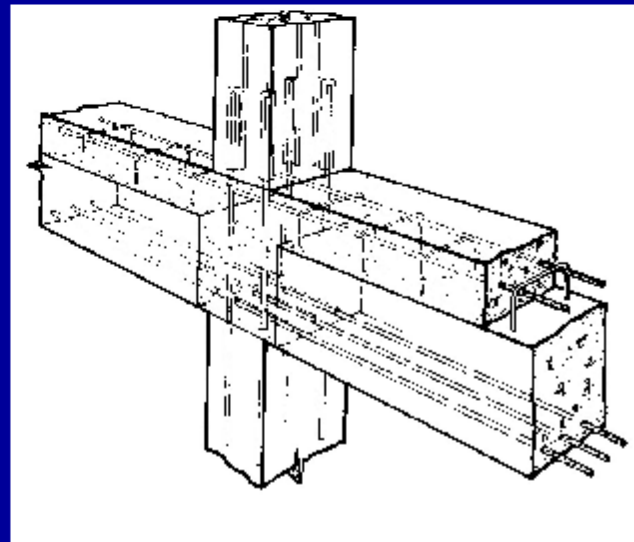
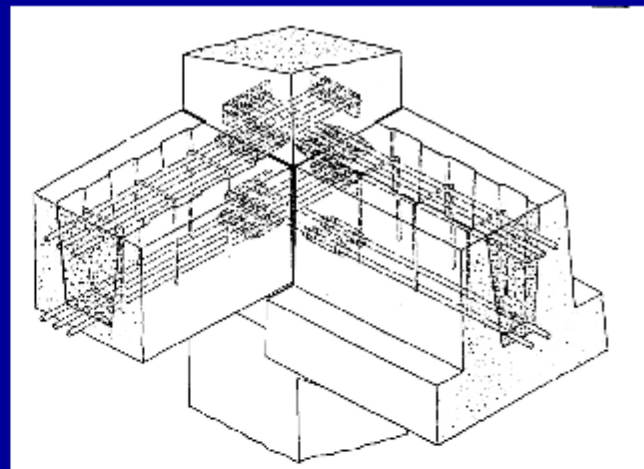
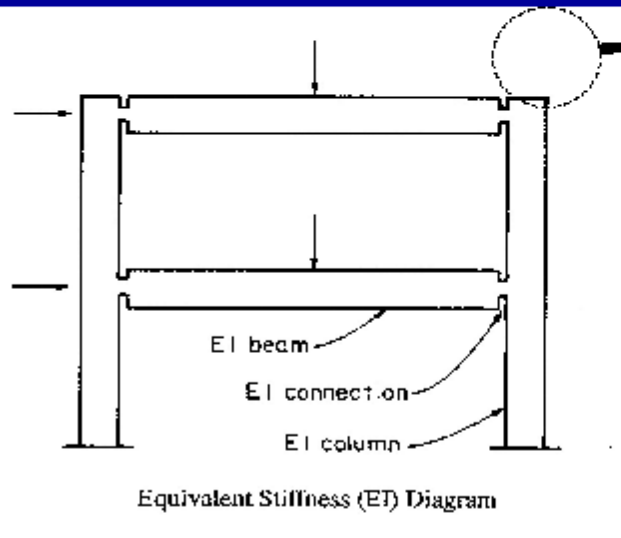
- Example of moment resisting frame system



Example of rigid
beam-to-column
connection

Frame Action – Moment Resistance Frame

- Other examples of rigid frames

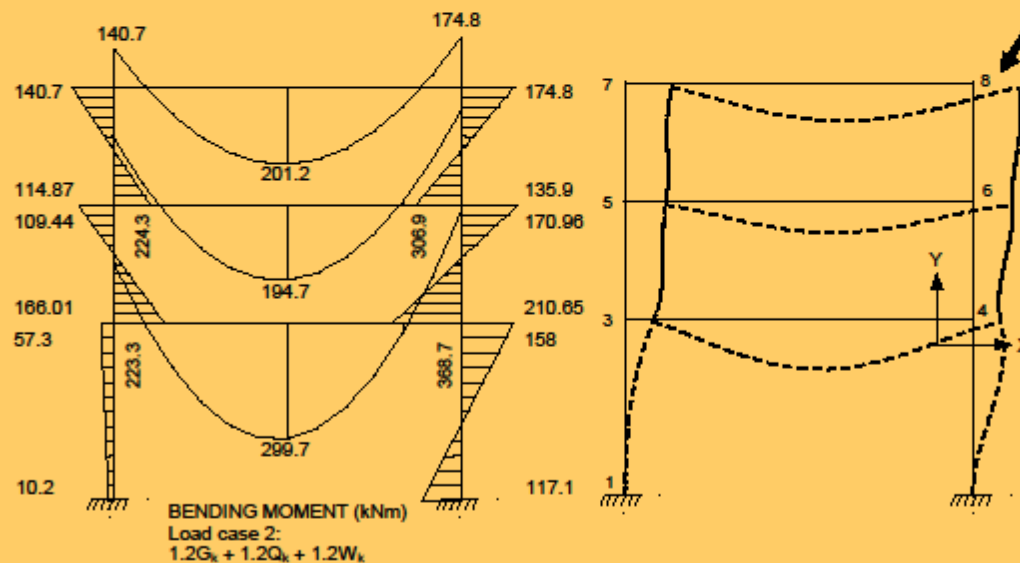


Beam Column Joint



Frame Action - Moment Resistance Frame

Results of analysis of bending moment
of resisting frames



The resistance to horizontal loadings is provided by the bending resistance of frame members and their connections

Frame Action – Moment Resistance Frame

Limitation:

- **Rigid beam-to-column connections, difficult to construct.**
- **Rigid base – foundation should be designed considering the moment.**

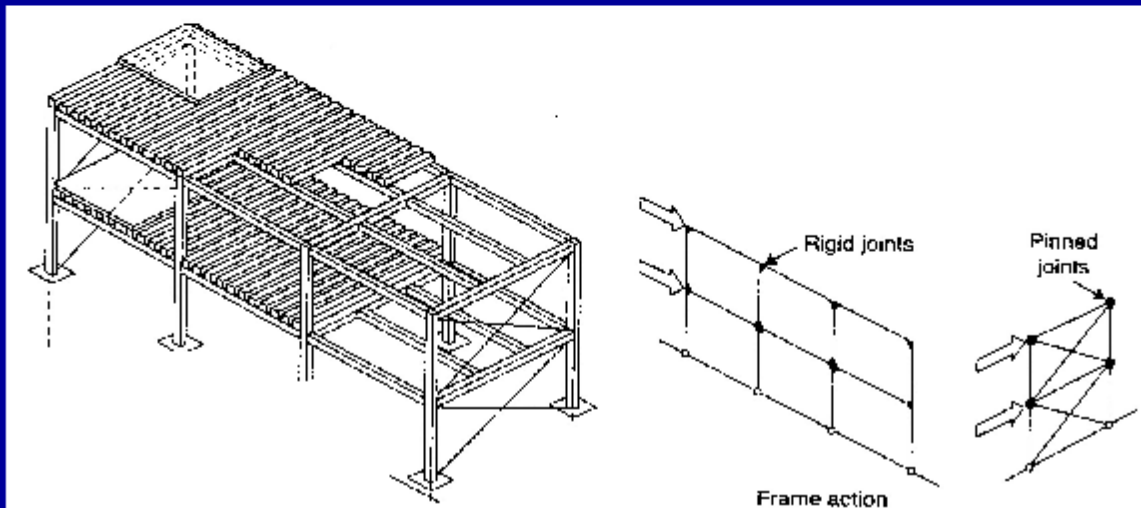
Advantages:

- **No bracing such as shear walls or cores.**
- **Suitable for low rise frames.**
- **Suitable for buildings in seismic regions.**

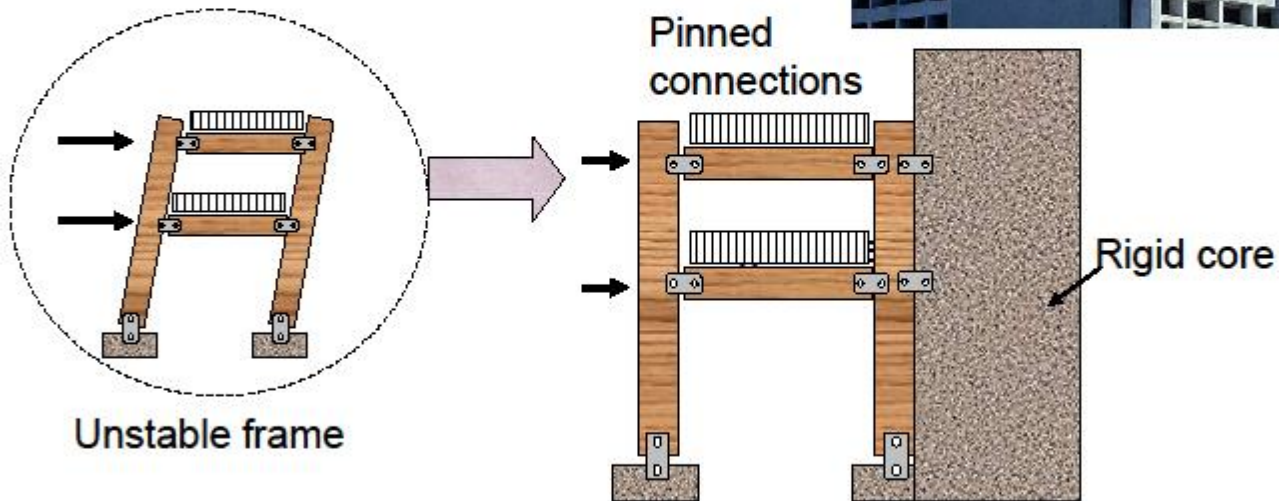
Independent lateral stability system

Skeletal braced frames (the skeletal frames are combined with other lateral stabilising components):

- In precast concrete structures, bracing elements are provided in the forms of shear walls).
- Other methods of bracings are infill brick walls or steel cross-bracing.



Frame Stability

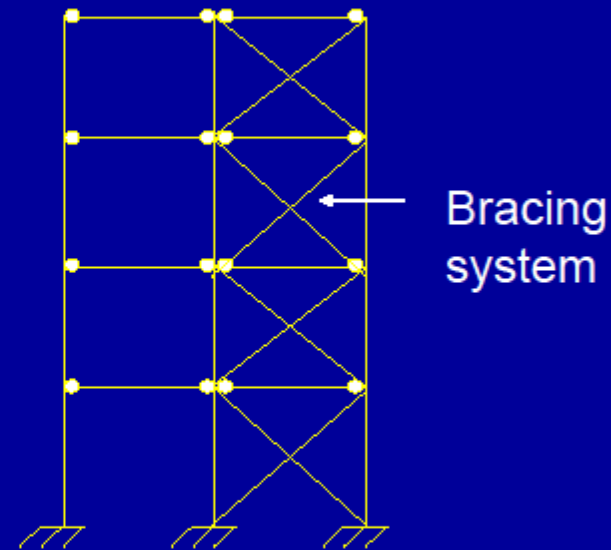


Frame is stabilized by rigid shear wall or RC core

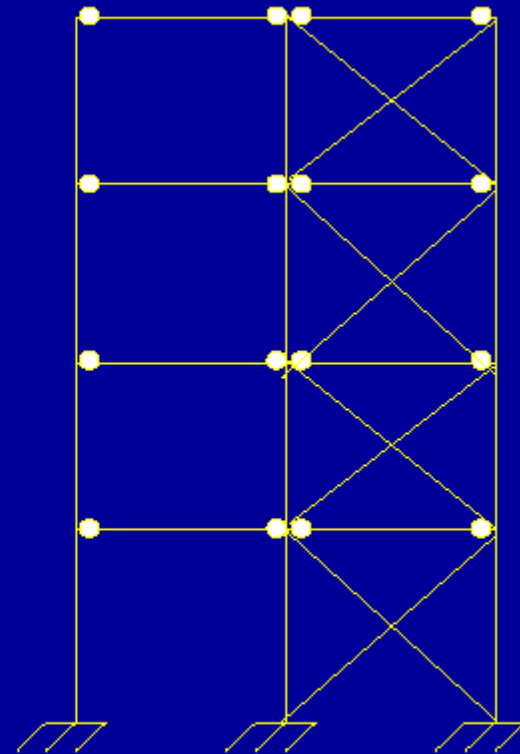
Shear wall

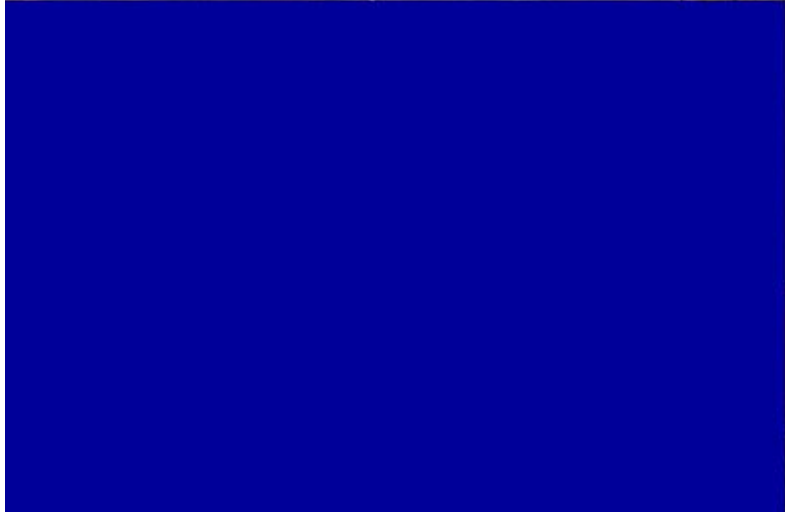
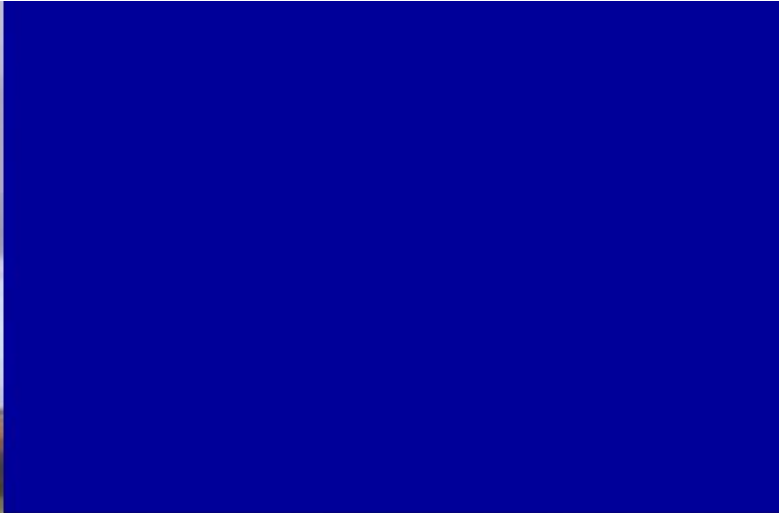
- **Shear walls act as vertical cantilever beams**
- **Shear walls transfer lateral forces from the superstructure to the foundation.**
- **In most precast, it is desirable to resist lateral loads with shear walls of precast or cast-in-place concrete.**
- **Shear walls can consist of the following:**
 - **Exterior wall system**
 - **interior walls**
 - **walls of elevator**
 - **cores**

- Precast skeletal structures of more than 3 storeys are normally braced.
- Precast concrete walls may be classified as infill or cantilever.



- In braced structures, pinned beam-to-column connections may be employed, hence connection details, design and construction are greatly simplified.





BRACED FRAME

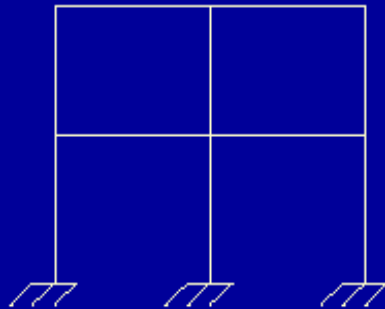
BRACING – precast cross bracing designed as fixed ended “struts”



SKELETAL FRAME SYSTEM

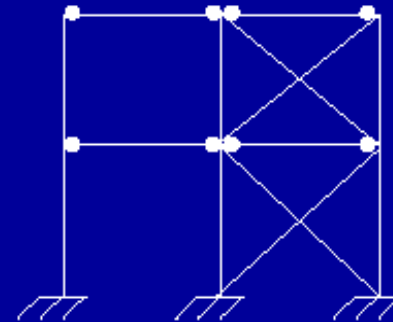


Unbraced Frames



In unbraced frame, the lateral forces are resisted by its own lateral stability such as cantilever columns or rigid frames.

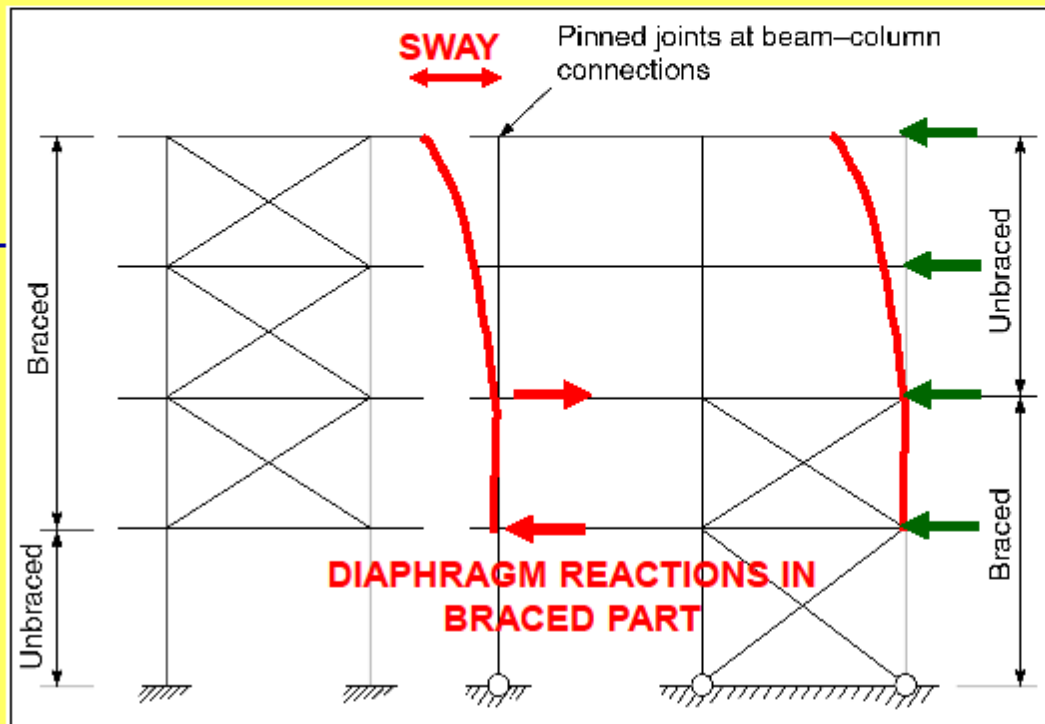
Braced Frames

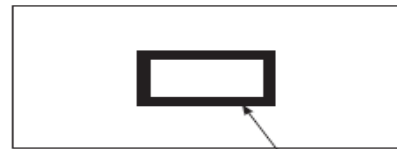


In braced frame, the lateral forces are resisted by lateral supports such as bracing, core or shear wall.

STABILISING METHODS

Partially braced – top up, or bottom down

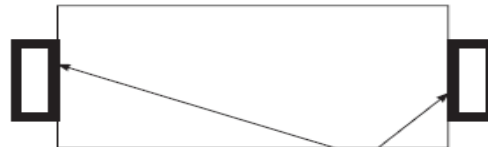




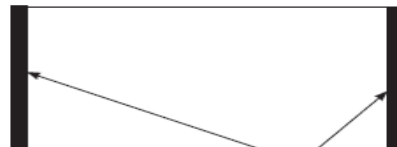
Central core gives maximum structural efficiency



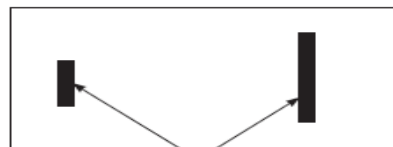
Eccentric cores are less efficient, but are possible



External symmetrical cores are very efficient



External symmetrical shear walls

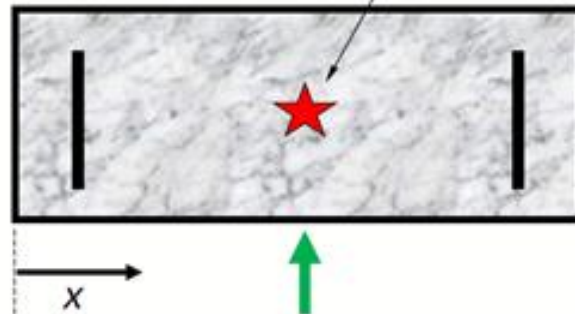


Internal non symmetrical shear walls

Determine the Centre of Frame Stiffness

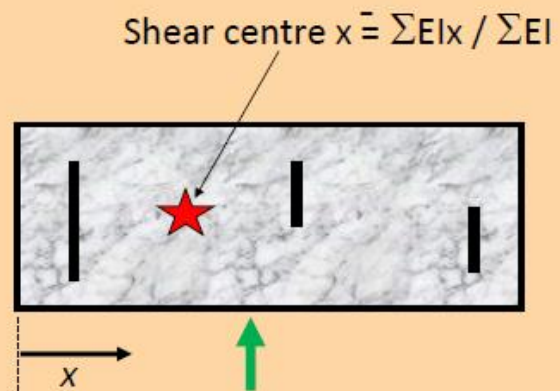
For symmetrical bracing $\bar{x} = \text{Mid-length } (L/2)$

Shear centre $\bar{x} = \Sigma EI x / \Sigma EI$



Where does net
reaction occur

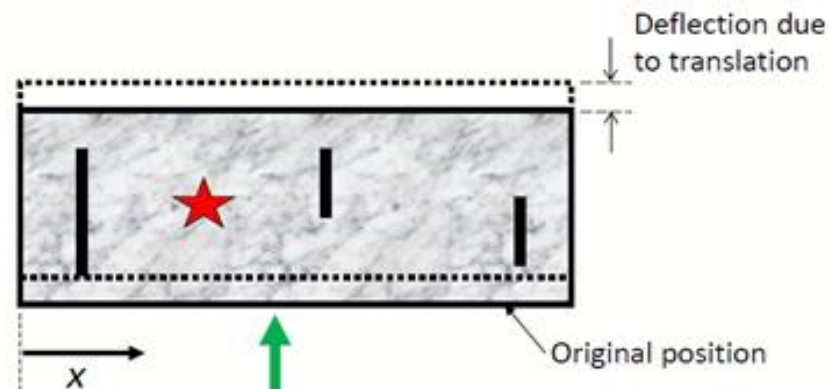
Determine the Centre of Frame Stiffness



Determine the Reactions in the Bracing/Shear Wall

Reaction in each wall due to 2 effects:

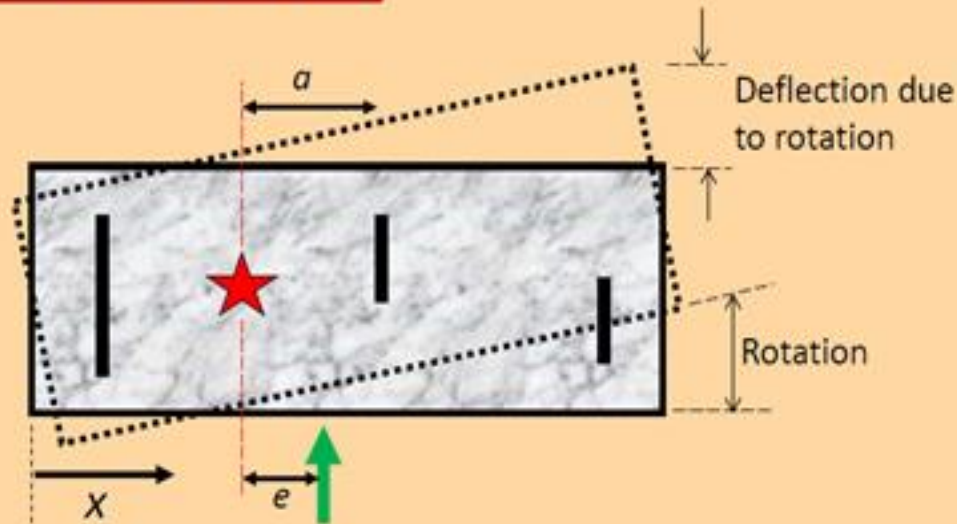
$$\frac{H_n}{H} = \frac{E_n I_n}{\sum E_i I_i}$$



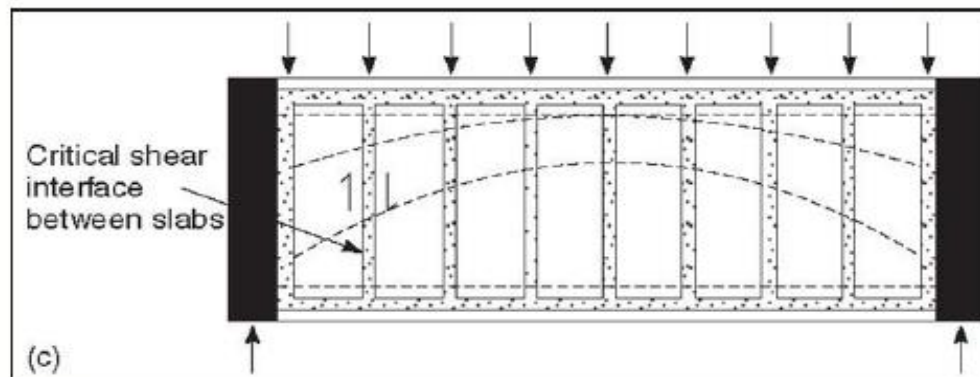
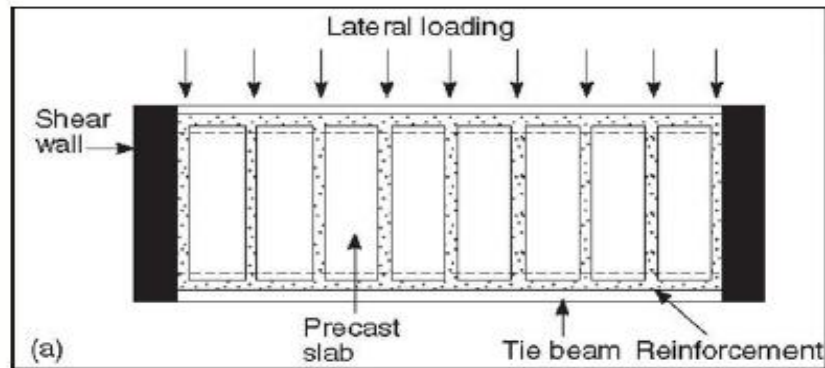
Determine the Reactions in the Bracing/Shear Wall

Reaction in each wall due to 2 effects:

$$\frac{H_n}{H} = \frac{E_n I_n}{\sum E_i I_i} \pm \frac{e E_n I_n a_n}{\sum E_i I_i a_i^2}$$



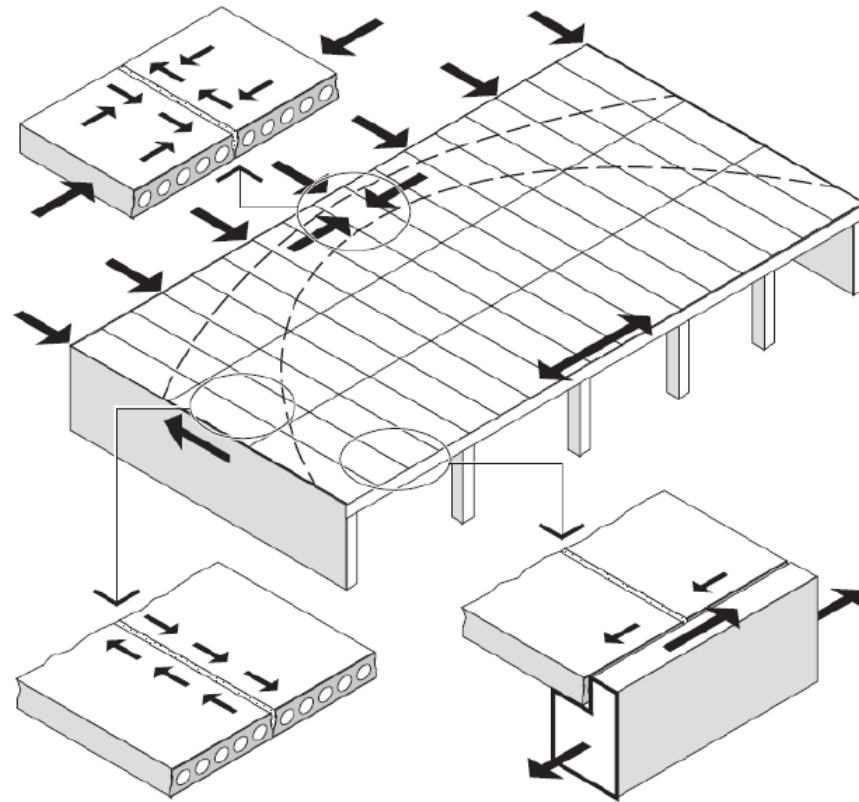
Structural Models



Structural Models

Horizontal Load Transfer by Diaphragm Action

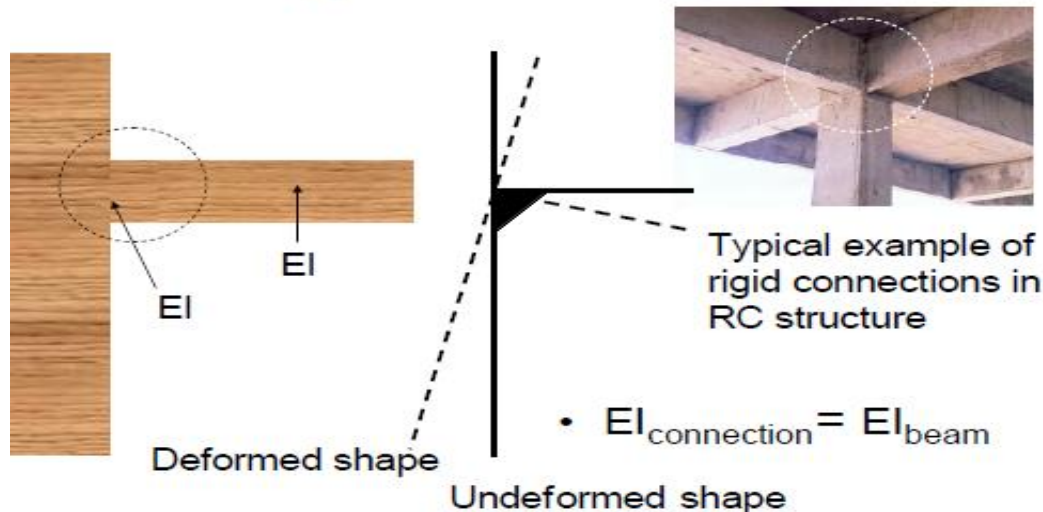
*(Hollowcore Flooring Technical Manual:
National Precast Concrete Association
Australia)*



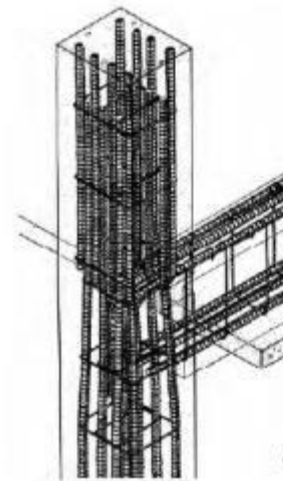
Rigid Connection

- Rigid connection are also called moment resisting connections
- Rigid connections are able to transfer moment and shear forces
- Best example of a rigid connection are

Rigid connection



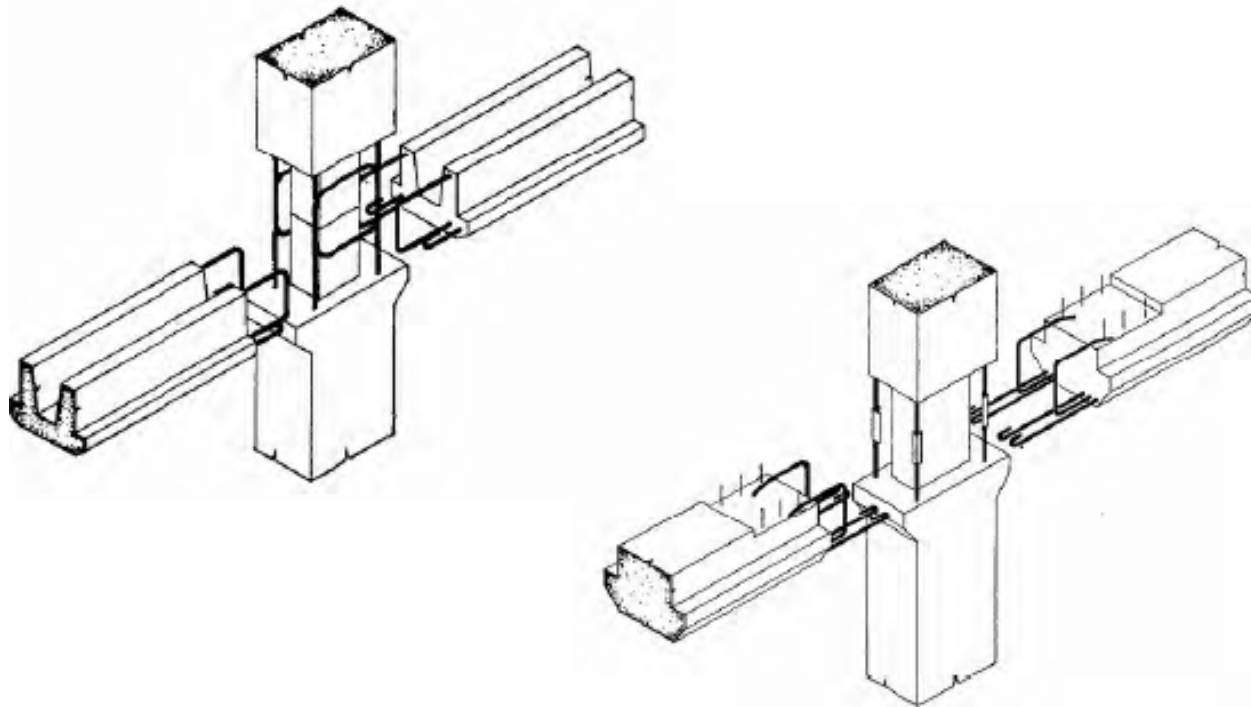
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Monolithic rigid connection in reinforced concrete frames

Rigid Connection

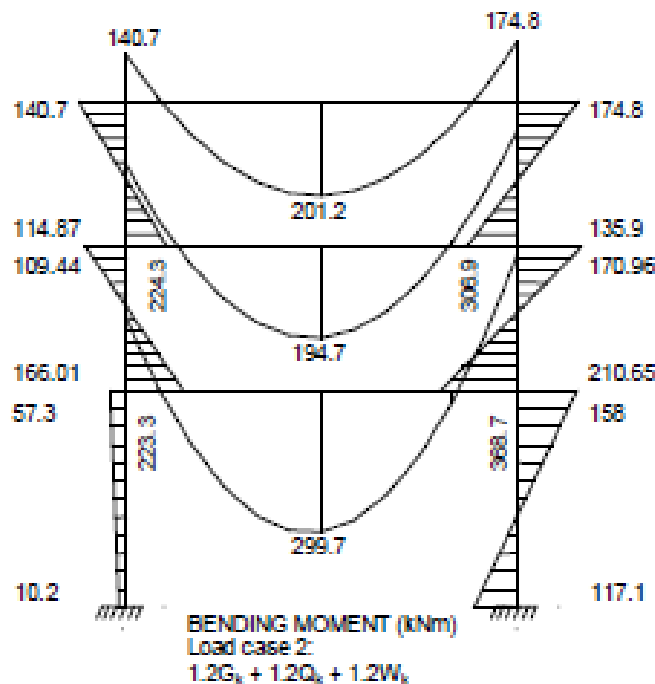
Rigid connection



- Rigid beam-to-column connection is formed by overlapping steel bars and insitu concrete

Rigid Connection

- Resultant applying rigid connections
 - Beam to column connections are able to re



CORBEL

- A corbel is a short cantilever projection from the face of a column (or wall) that supports a loadbearing component on its upper horizontal ledge.
- Mostly use on columns
- Care is needed to ensure proper contact surface and anchorage to contact surface fixing tolerances

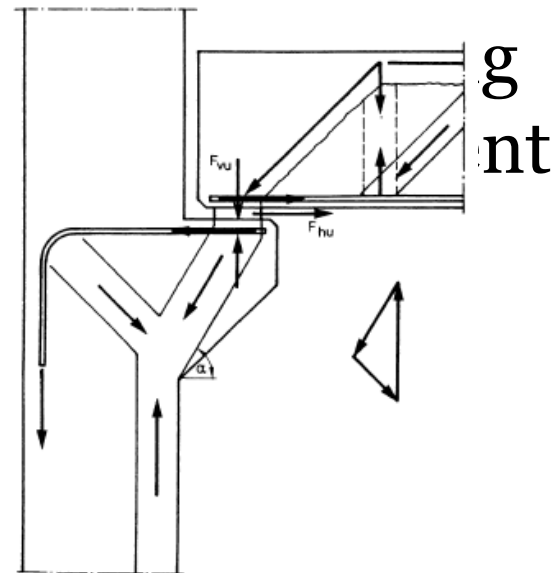


Figure 7.92 Shear force transfer between beam end and column corbel [7.18].

CORBEL

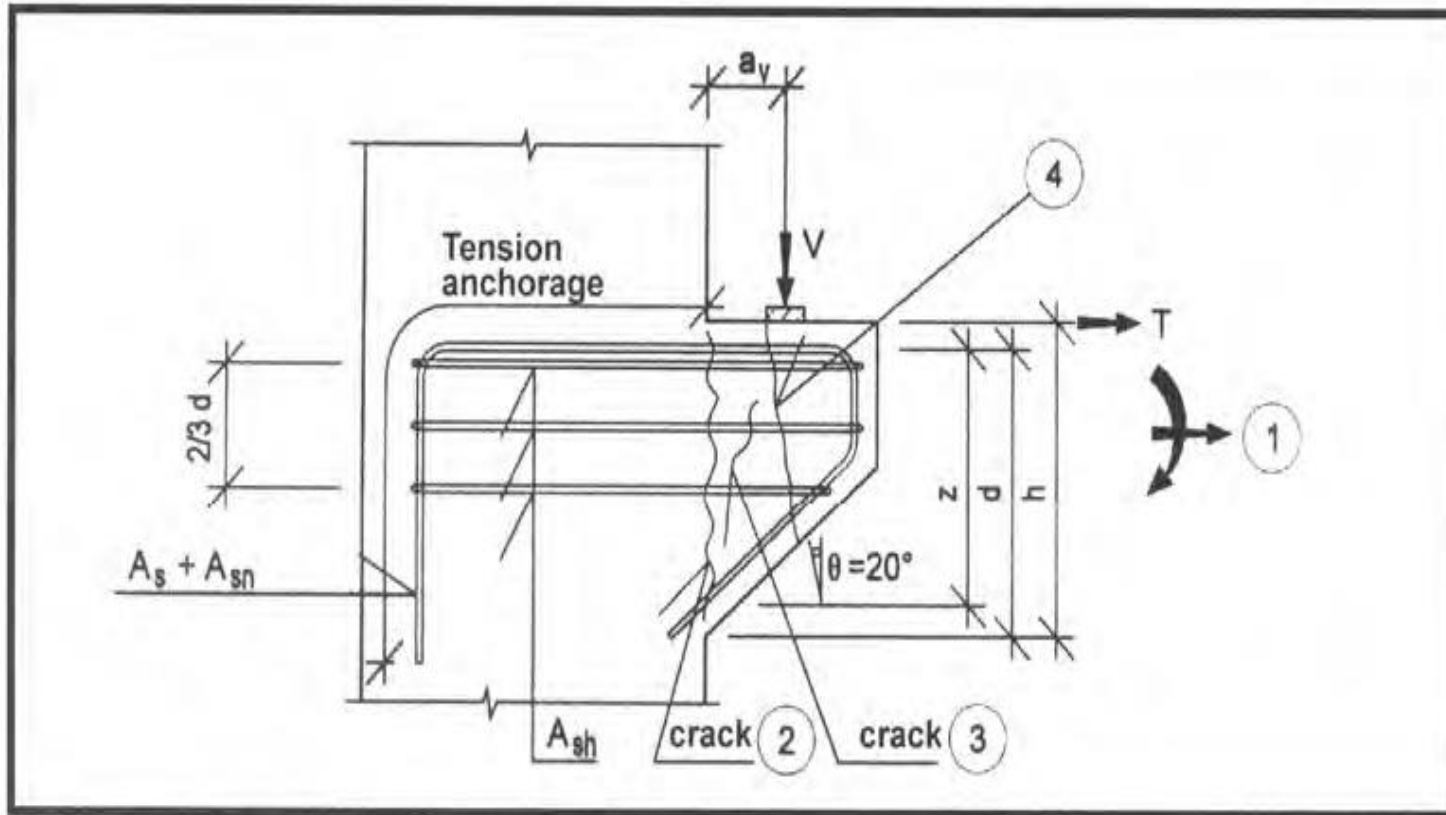
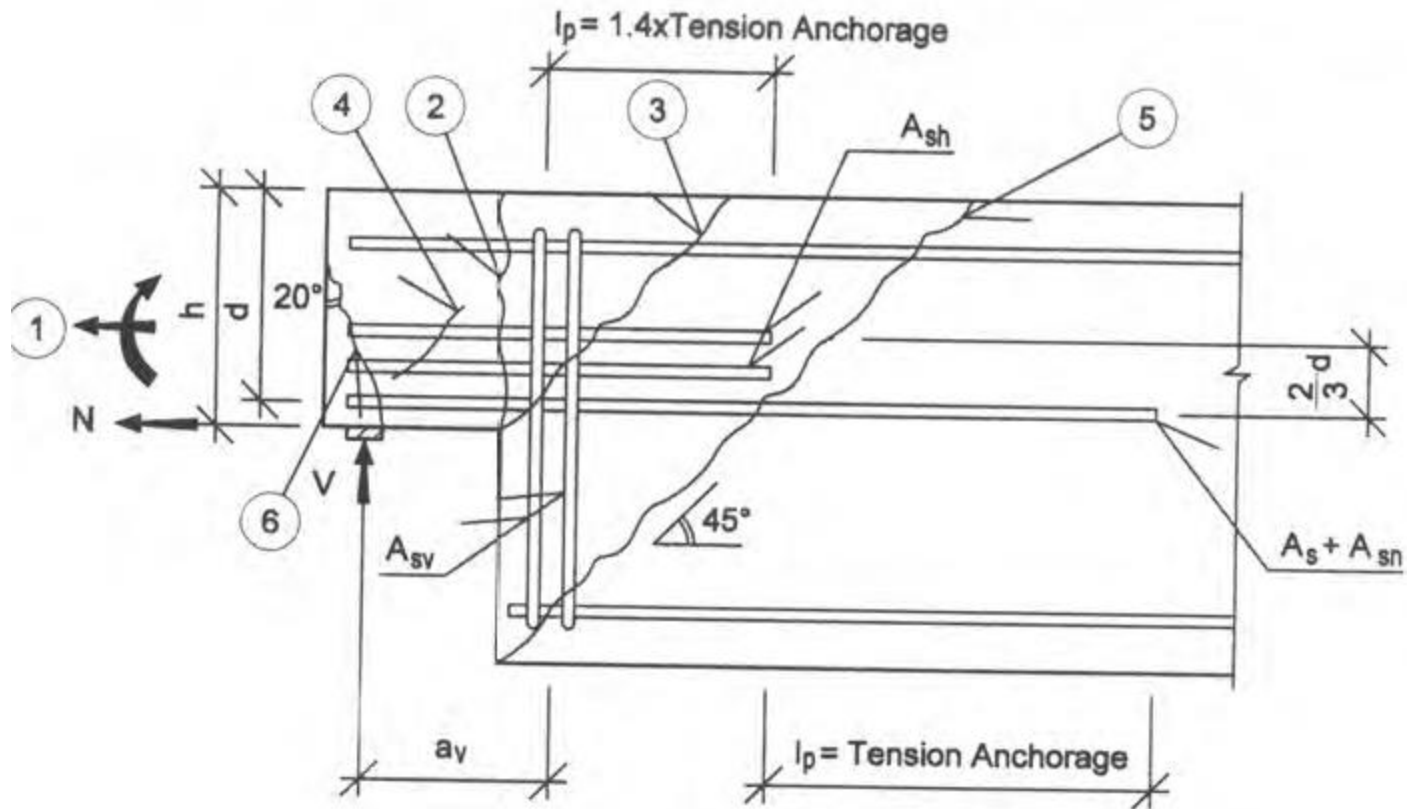


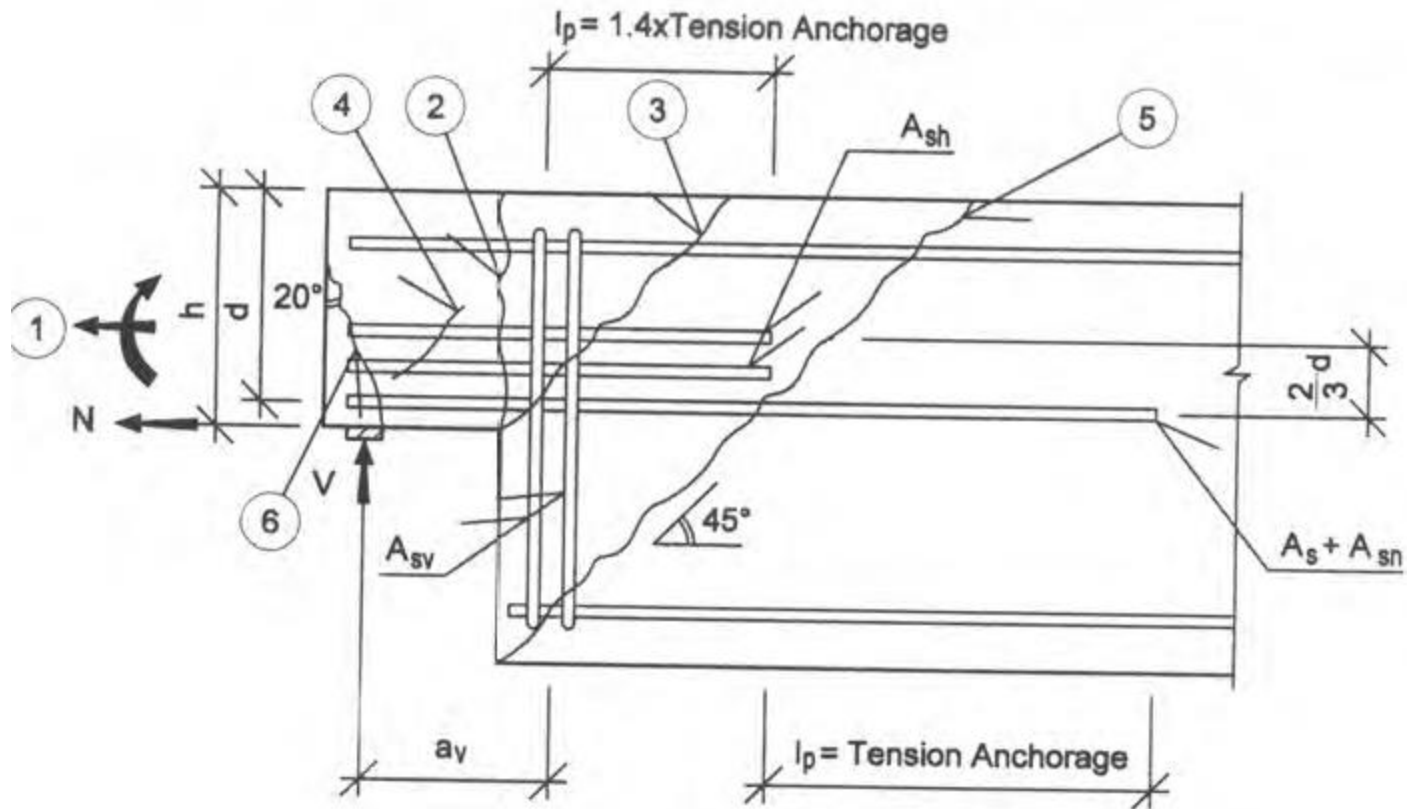
Figure 3.12 Potential Cracks In Corbel

Half Joint Beam



(a) Schematic reinforcement

Half Joint Beam



(a) Schematic reinforcement



● Full Corbel design

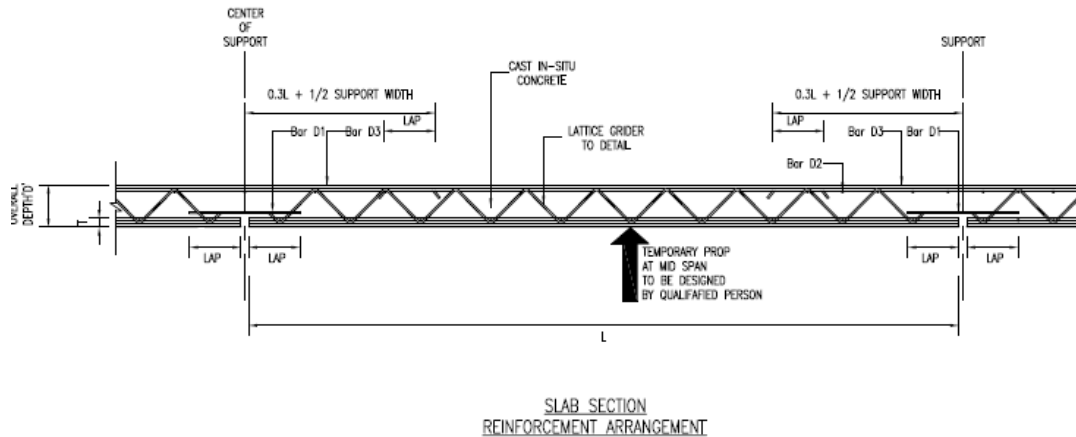
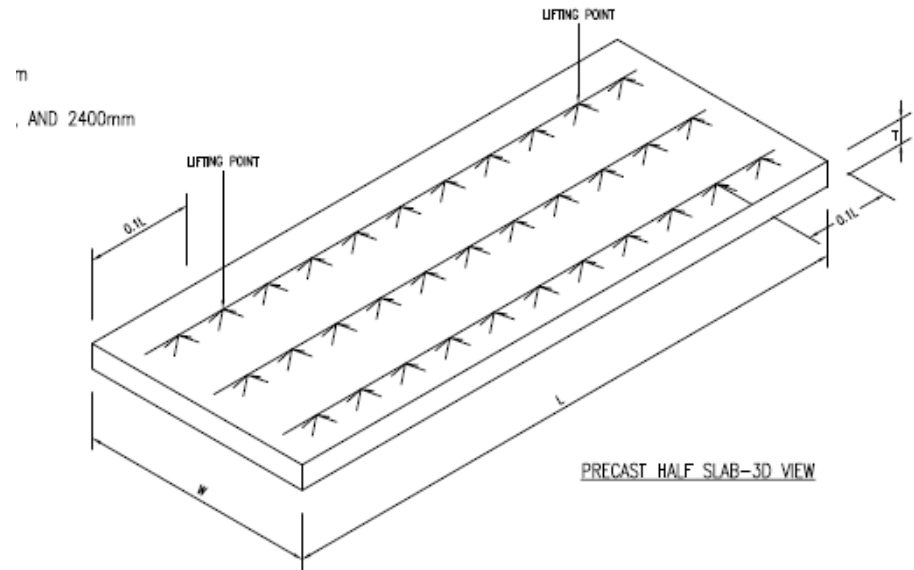
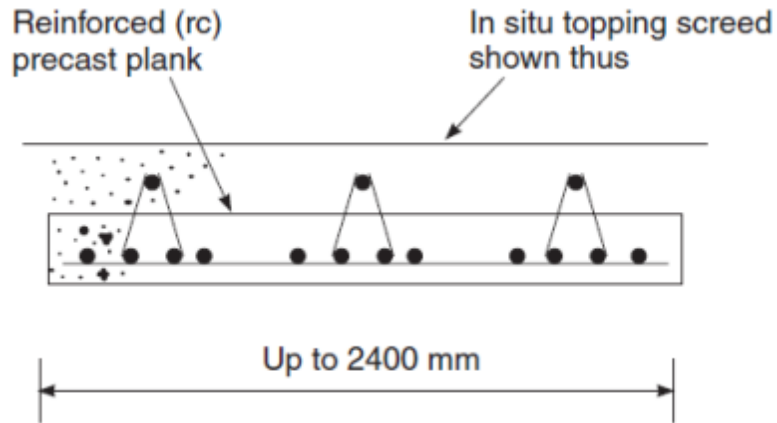


- Hidden Corbel and Half Joint beam design



- Hidden Corbel and Half Joint beam design

Precast Half Slab



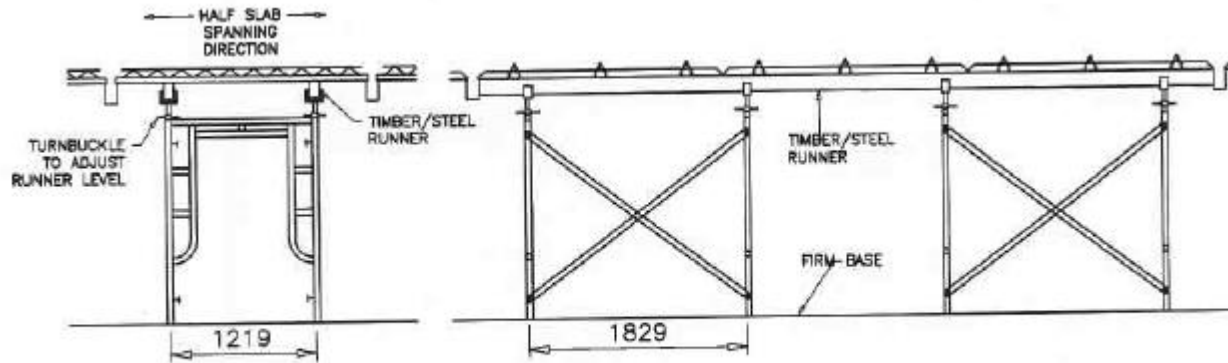


Figure 15 Temporary props for half slab erection

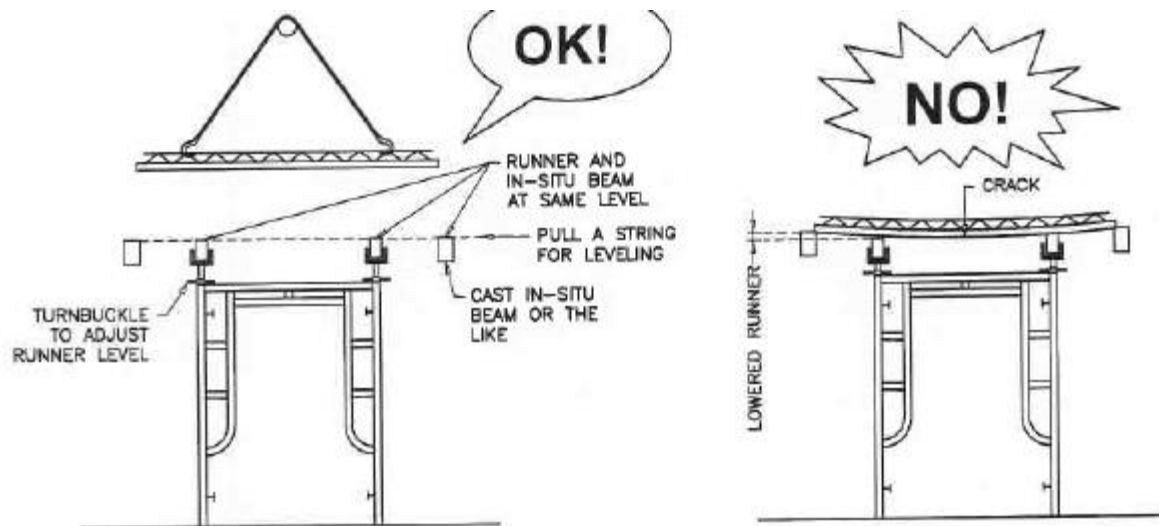


Figure 16 Proper and improper placement of prop

- Extract From Hume Industry Method Statement

- 3 The sequence of fixing floor slabs should be continuous in one direction commencing from the frame stabilizing elements, e.g. shear wall.
- 4 Place the half slabs across the beams and the well set scaffold in accordance to the approved construction drawing. Care should be taken at the end bearing length on beams. Any significant discrepancy, e.g. unable to reach the support or clash with the reinforcement beyond adjustment shall be reported to the Designer immediately for further instruction.
- 5 Bend down the starter bars from the beams into slab as shown in the following figure when the placing of slab fulfill bearing and elevation tolerance requirement.

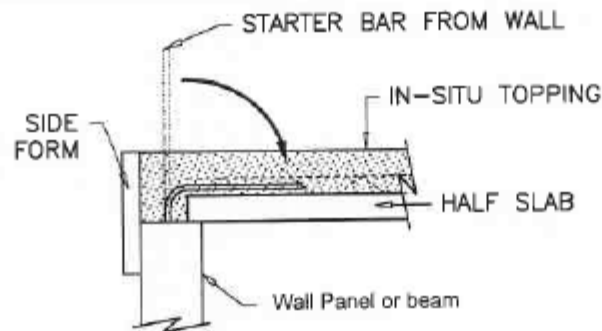


Figure 17 Starter bars from wall

● Extract From Hume Industry Method Statement



● Precast Half Slab Production di MTD ACPI



● Precast Half Slab Production di MTD ACPI



- Precast Half Slab Production di MTD ACPI



- Gambar Menunjukkan Precast Half Slab Production di Corporate Builders



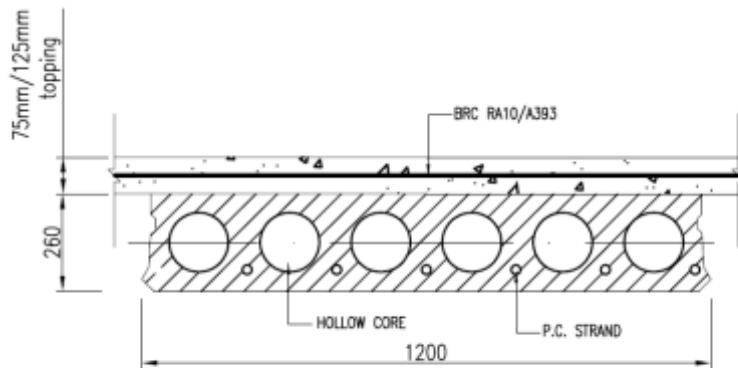
- Precast Half Slab Yang Telah Dipasang di Balai Polis Sungai Dua (MTD ACPI)



- Precast Half Slab Yang Telah Dipasang di Balai Polis Sungai Dua (MTD ACPI)

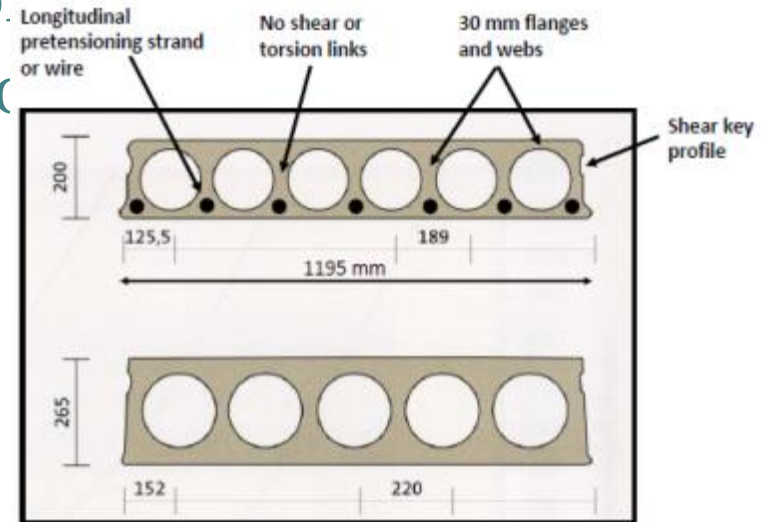
Precast Hollow Core Slab

- characteristics
 - 400-3600mm wide, typically 1200mm
 - 90-730mm deep; typically 150,200,250,300mm
 - Selfweight 1.5 to 5.0 kN/m²



PRECAST PRESTRESSED HOLLOW CORE SLAB

of solid section
10



Precast Hollow Core Slab

DL/Action

| | | | |
|-----------------------------------|---|------|-------------------|
| Brickwall on HC Slab | = | 2.60 | kN/m ² |
| 75mm conc topping | = | - | kN/m ² |
| 100 mm conc topping for levelling | = | 1.25 | kN/m ² |
| Finishes+Ceilings+M&E | = | 1.80 | kN/m ² |
| HC Slab Selfweight | = | - | kN/m ² |
| <u>TOTAL DL</u> | = | 5.65 | kN/m ² |

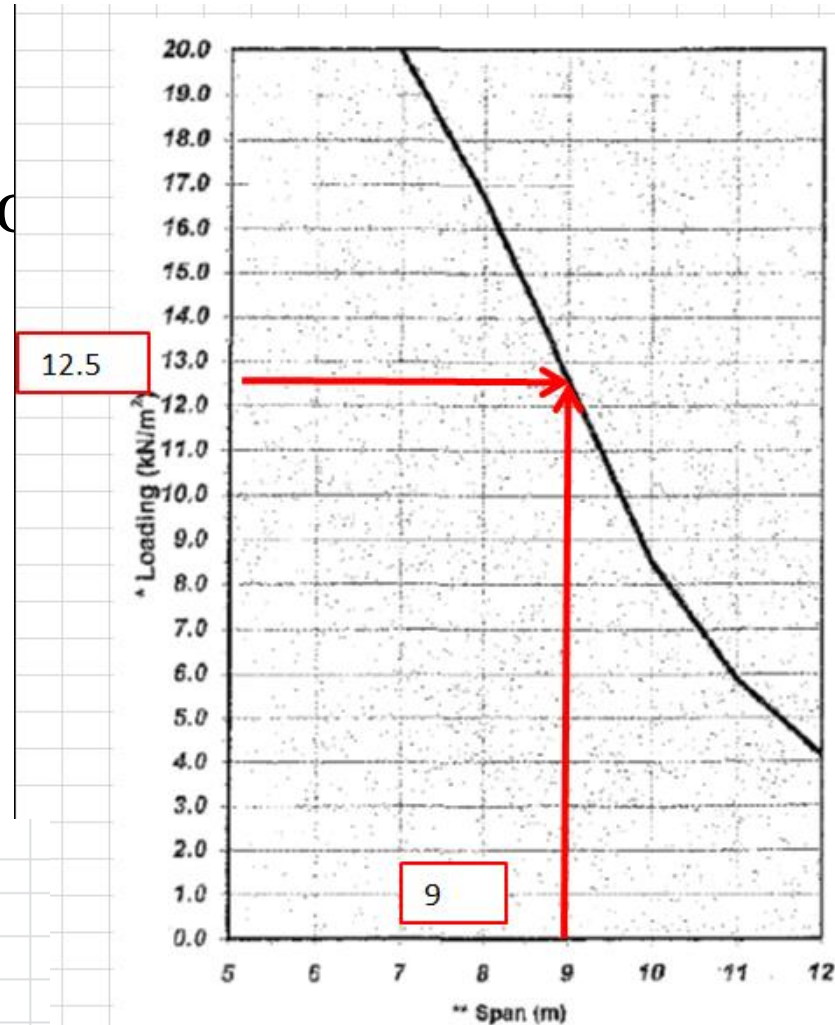
LL/Variable = 5.00 kN/m²

Total DL+LL = 10.65 kN/m²

Actual Length of of HC Slab

| | | | |
|------------------------------------|---|------|----|
| Longest Grid to Grid | = | 9.30 | m |
| Assume Inverted T /Edge Beam Width | = | 300 | mm |
| Actual Length of HC Slab | = | 9.00 | m |

elc





TERIMA KASIH